

Fabrication of GRCop-84 Rocket Thrust Chambers
by
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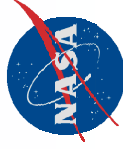
GRCop-84, a copper alloy, Cu-8 at% Cr-4 at% Nb developed at NASA Glenn Research Center for regeneratively cooled rocket engine liners has excellent combinations of elevated temperature strength, creep resistance, thermal conductivity and low cycle fatigue. GRCop-84 is produced from pre-alloyed atomized powder and has been fabricated into plate, sheet and tube forms as well as near net shapes. Fabrication processes to produce demonstration rocket combustion chambers will be presented and includes powder production, extruding, rolling, forming, friction stir welding, and metal spinning. GRCop-84 has excellent workability and can be readily fabricated into complex components using conventional powder and wrought metallurgy processes. Rolling was examined in detail for process sensitivity at various levels of total reduction, rolling speed and rolling temperature representing extremes of commercial processing conditions. Results indicate that process conditions can range over reasonable levels without any negative impact to properties.

Fabrication of GRCop-84 Rocket Thrust Chambers

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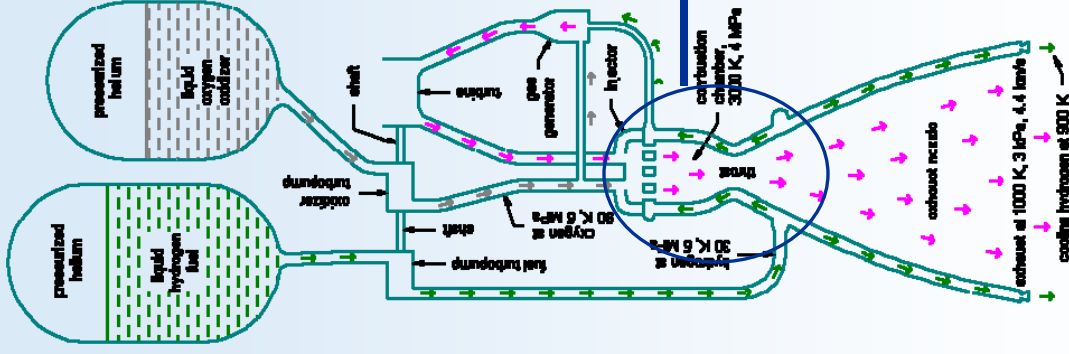


Fabrication of GRCop-84 Rocket Thrust Chambers

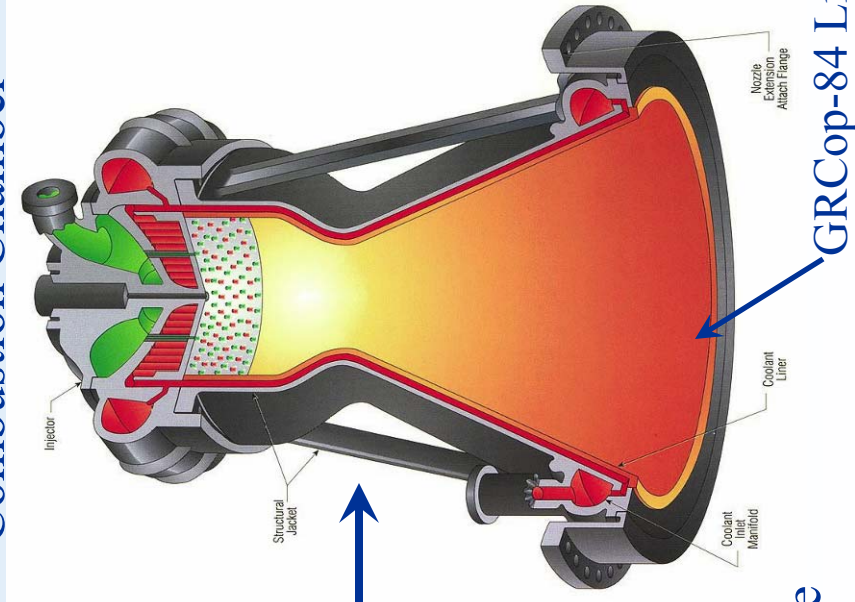
Outline

- Rocket Thrust Chambers
- GRCop 84 Properties
- Thrust Chamber Fabrication Steps
- Warm Rolling Optimization
- Conclusions

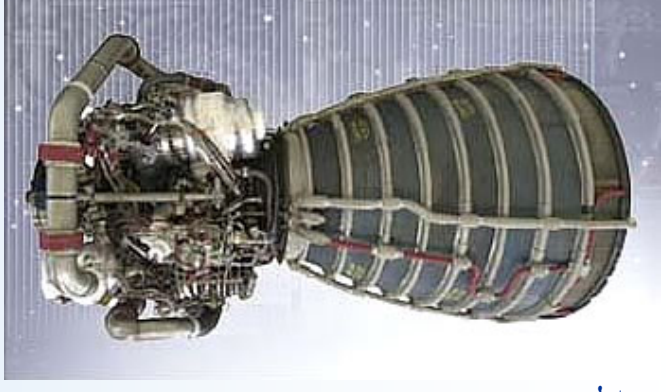
Rocket Thrust Chambers



Combustion Chamber



Shuttle Main Engine



Regen Cool Rocket Engine

Ref: www.islandone.org/LEOBiblio/SPBH101.HTM

Glenn Research Center at Lewis Field

Why GRCop84 for Rocket Thrust Chambers?

GRCop-84 (Cu-6.5 Cr 5.8 Nb)
Stable dispersion of Cr₂Nb

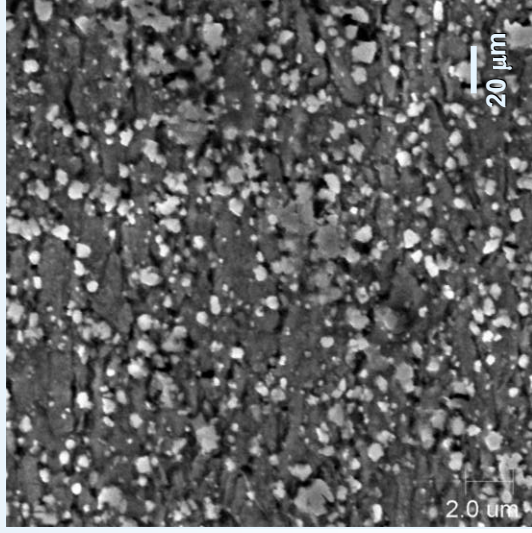
Competitive Alloys

OFHC Cu (Cu) - Can be work hardened

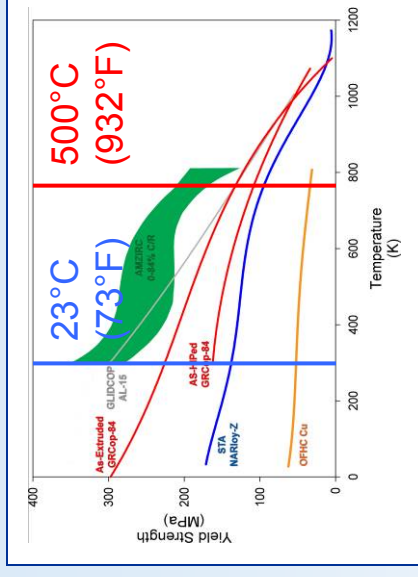
AMZIRC (Cu-0.15Zr) - Precipitation and work hardened alloy

GLIDCOP (Cu-0.15 to 0.60 Al₂O₃)
Dispersion strengthened alloys

NARloy-Z (Cu-3 Ag-0.5 Zr) - Precipitation strengthened alloy, Current Space Shuttle Main Engine (SSME) liner material

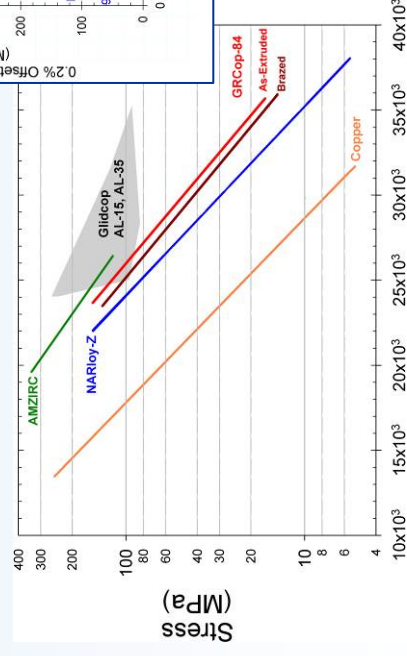


Typical rolled microstructure

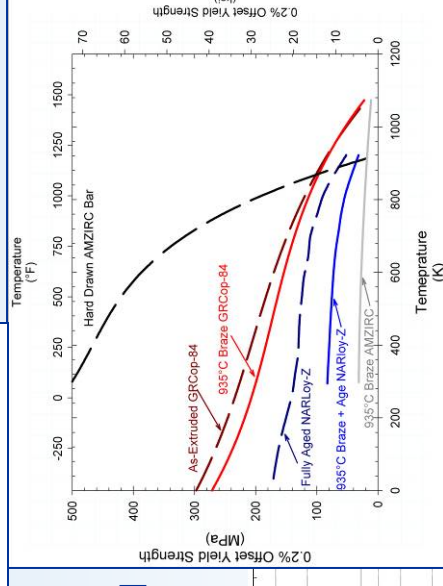


Excellent elevated
temp strength

Retains strength after
935°C (1715°F) simulated
braze cycle



Superior creep
strength



Larson-Miller Parameter
 $T(^{\circ}R) * [\log_{10}(t(h)) + 17]$



Major Fabricating Steps Rocket Thrust Chamber

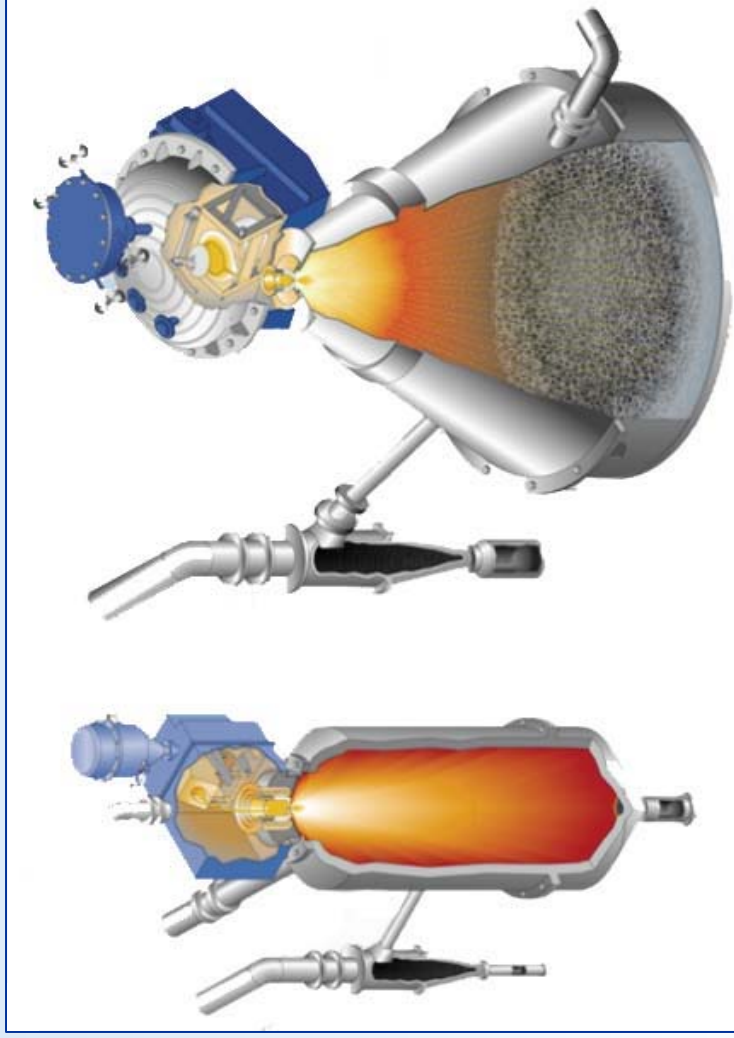
Demonstrated Processes

1. Powder Production
2. Canning
3. Extrusion
4. De-can and Billet Prep
5. Roll/Anneal/Clean
6. Form Half Cylinders
7. Friction Stir Weld
8. Metal Spin
9. Anneal
10. Machine ID, rough OD
11. Coat Liner w/ NiCrAlY and HIP
12. Machine ID + OD Cooling Channels
13. Closeout (Ni) and Machine
14. Assemble MSFC Jacket and Manifolds
15. Hot Fire Testing

Future Work
2006 ➡

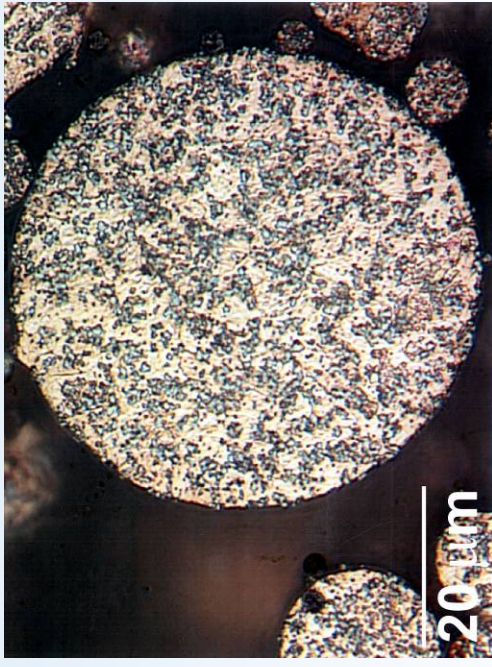
Production Of GRCop-84 Powder

(Crucible Research, Pittsburgh, PA)



**Laboratory Gas
Atomizer**
50 pound capacity

**Pilot Gas
Atomizer**
300 pound capacity



Typical Powder
-140 mesh ($<106\text{ }\mu\text{m}$)
Average diameter 35-40 μm

Canning And Extrusion

(Crucible Research, Pittsburgh, PA and HC Starck, Coldwater, MI)



15.1" Diameter Copper Can
800-1,200 pounds
of GRCop-84 powder



Hot Extrusion
2.9" x 9.9"



**GRCop-84 can be extruded at low (7:1)
to high (60:1) reductions in area**

Billet Sawing, Flattening and Decaning

(Lunar Tool and Mold, Cleveland, OH)



As-extruded with copper can



After Milling top and bottom surfaces
to remove copper can



Plate Rolling

(HC Starck, Euclid, OH)



GRCop-84 can be warm rolled or cold rolled.
Cold reductions to 90% demonstrated.



Entering rolling mill

After rolling, annealing and cleaning

GRCop-84 Plate

Rolled to approximately 0.525" x 20" x 54"
Each plate makes 1.5 to 2 liners

Half Cylinder Forming

(Spin Tech, Paso Robles, CA)



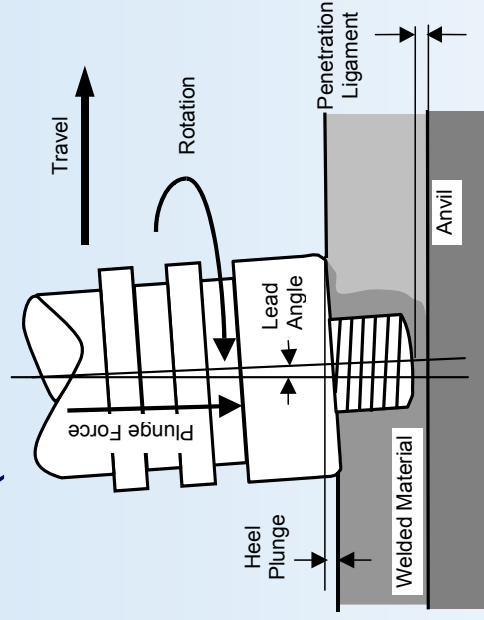
Forming plate into a half cylinder

GRCop-84 Half Cylinders
Nominally 5.5" id x 18" long



Friction Stir Welding

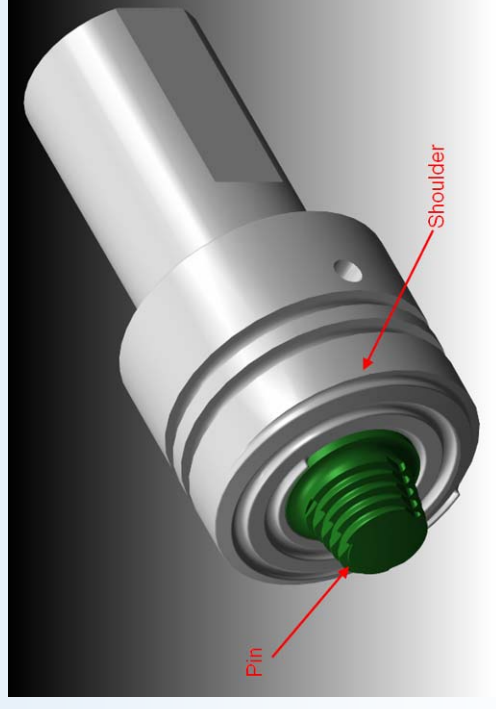
(NASA Marshall Space Flight Center, Huntsville, AL)



- **Solid state process – does not melt base metal**
 - Frictional heating from rotating pin locally plasticizes material at the joint
 - Applied load reacted by an anvil forges the material creating a weld
 - Three process parameters – rotation, load, and travel



GRCop-84 Welded Cylinder



Pin tool design and material
selected for specific application

Photos courtesy of NASA MSFC

Metal Spinning (Spin Tech, Paso Robles, CA)



Hot Metal Spinning over shaped mandrel



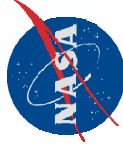
Before and after spinning



Liners were annealed at 600°C
to relieve residual stresses

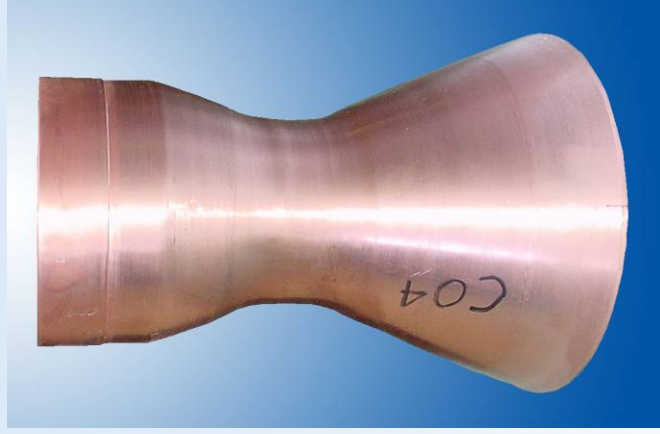
Photos courtesy of Spin Tech

Glenn Research Center at Lewis Field



Machining, Plasma Spray Coating

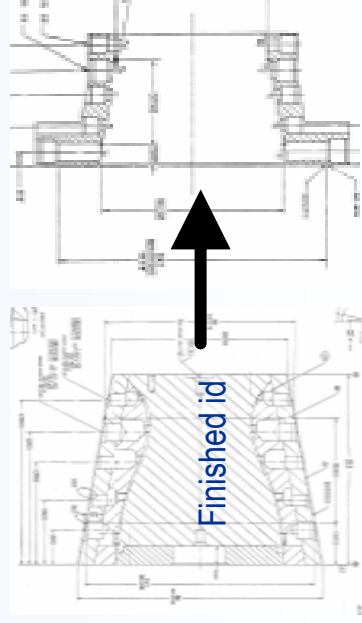
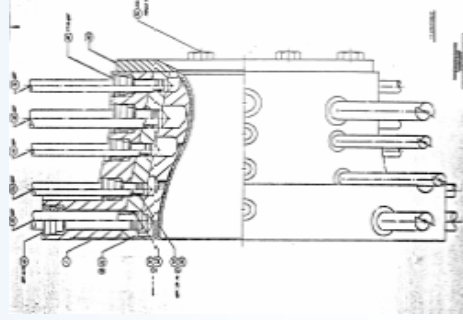
(Starwin Industries, Dayton, OH; Plasma Processes Inc., Huntsville, AL)



**Machined
Preform
ready for
coating**



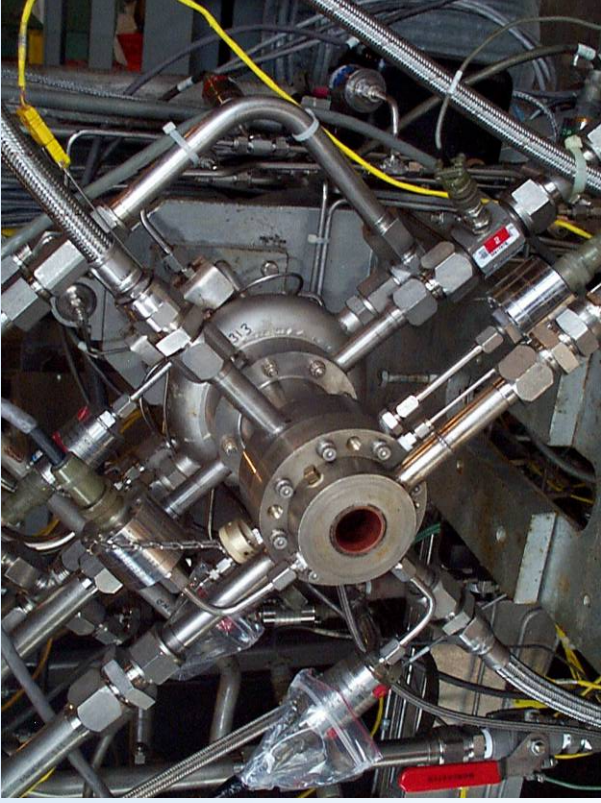
**Coated copper mock-up liner
Coating: Cu-8Cr-1Al Bond coat
and NiCrAlY top coat**



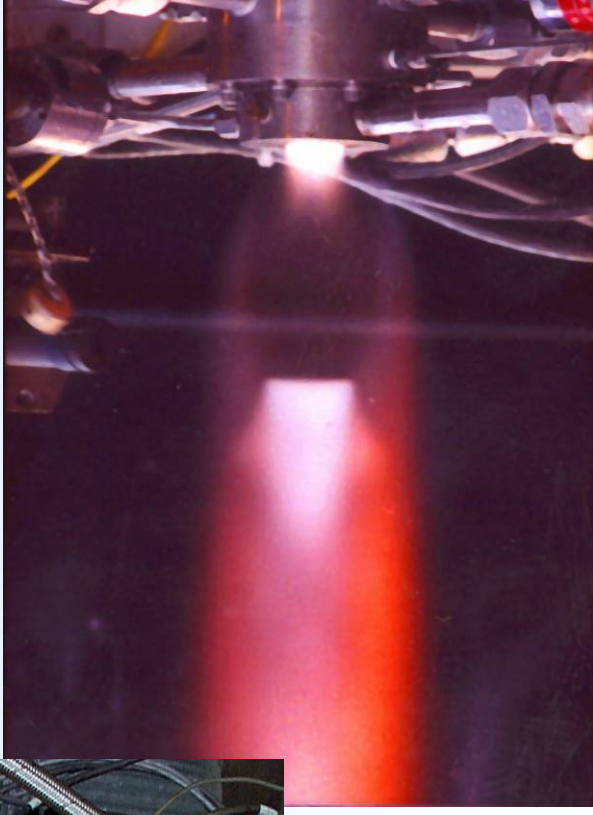
**Final machining, closeout
and installation into
calorimeter hardware for
hot fire testing.**

Hot Fire Testing

(NASA Marshall Space Flight Center, Huntsville, AL)



**GRCop-84 Hot Fire Test
in GRC Tests Cell 22
MSFC test configuration
will look very similar**



Warm Rolling Optimization

Examined the influence of total reduction, rolling speed, rolling temperature and a post-rolling annealing heat treatment of GRCop-84 on mechanical properties .
The interrelationships of these variables defines boundaries for a robust commercial rolling process.

Experimental Design

Rolling Temperature

215, 300 and 415 C

Rolling Reduction

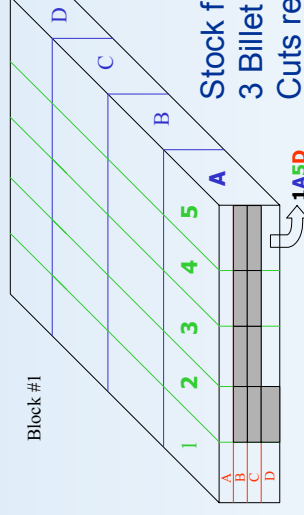
65, 95 and selected 99 %

Rolling Speed

69 and 217 f/min.

Heat Treatment (anneal) after Rolling:

none, 450C, selected 350 and 250C



Block Preparation

Stock from HC Stark Extrusion Runs #1 and #2
3 Billet ends were cut into small plates
Cuts removed copper extrusion can
Identified per schematic

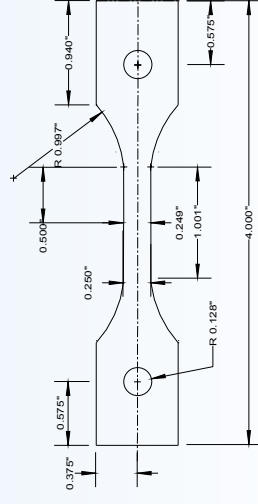
Strip Rolling Procedure

Rolled at HC Stark - Small Lab Mill

Reheat after every roll pass

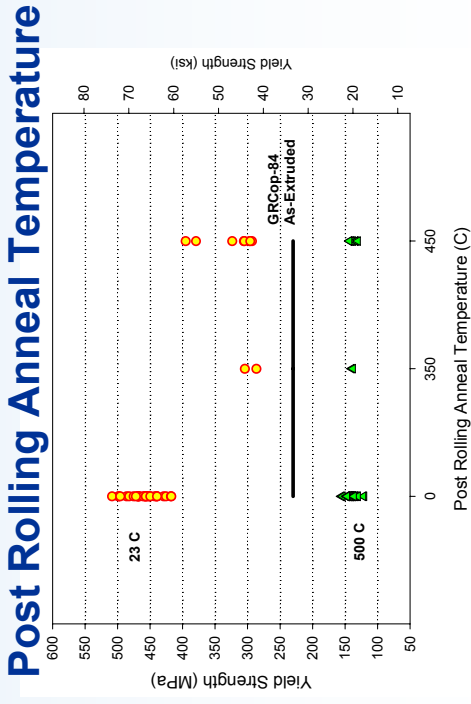
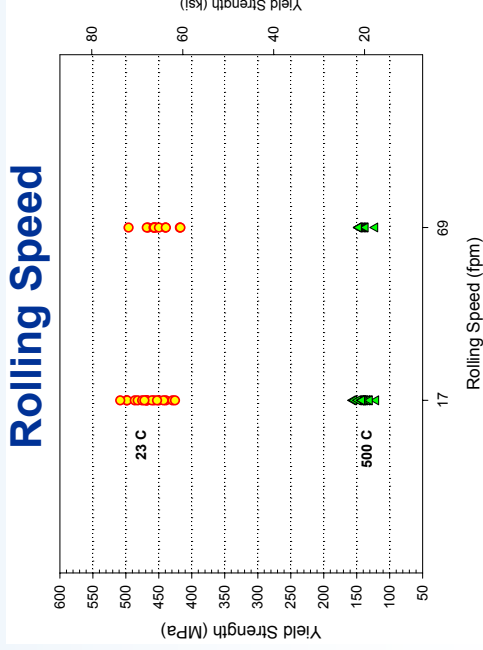
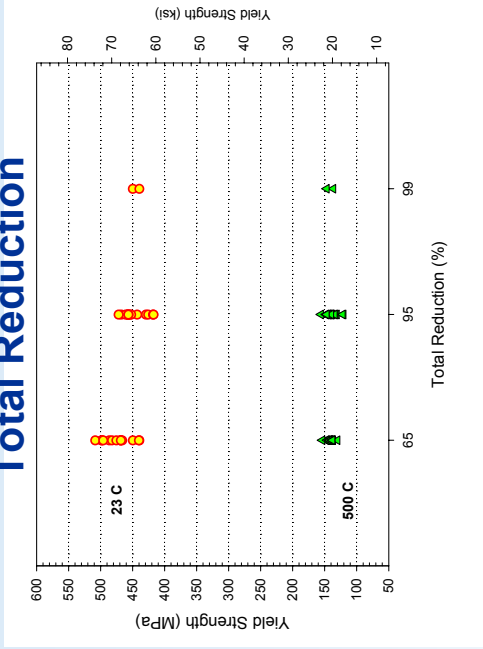
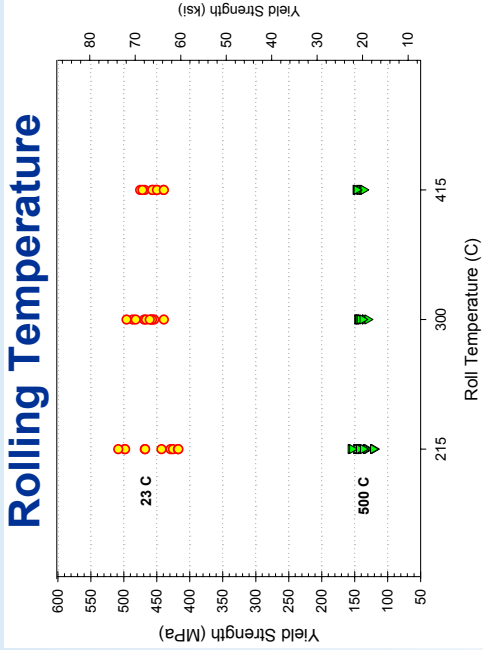
approx 20 min

Post rolling heat treatment on selected specimens at 250, 350, 450 C



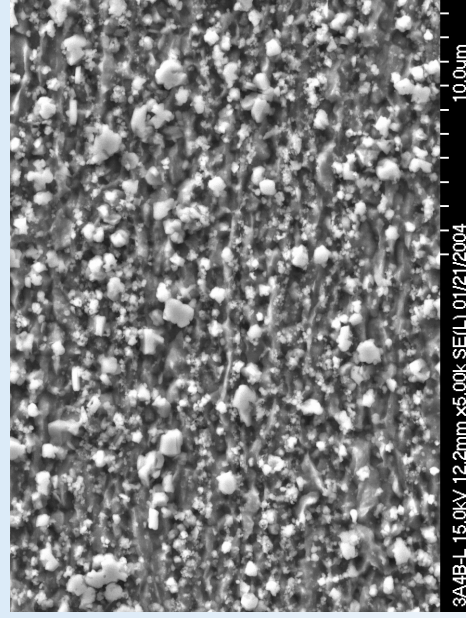
Test Specimens Per ASTM E8

Warm Rolling Optimization

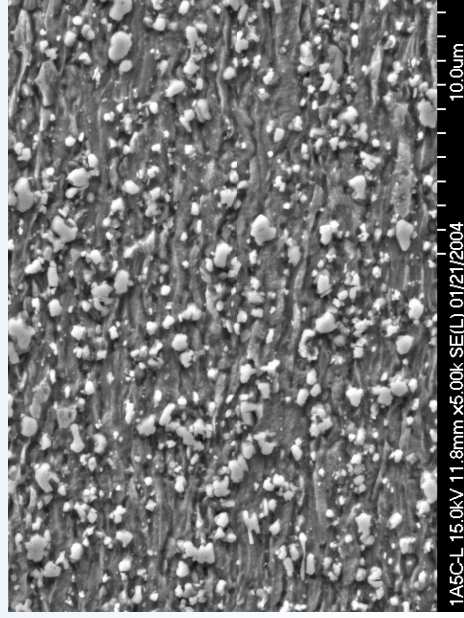


Warm Rolling Optimization

Metallography

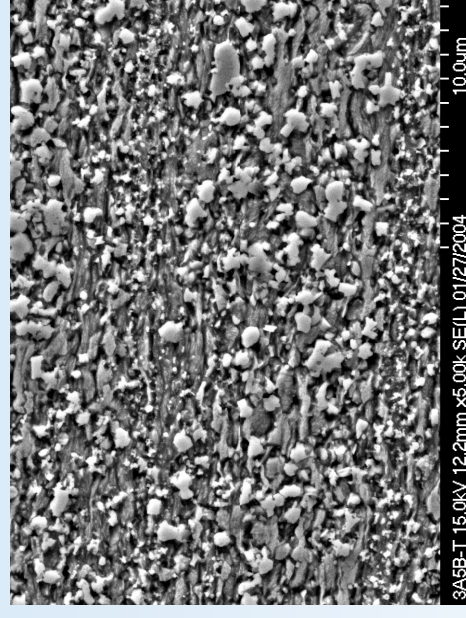


Roll Temp = 215 C, Total Red = 95 % , Roll Spd = 17 fpm

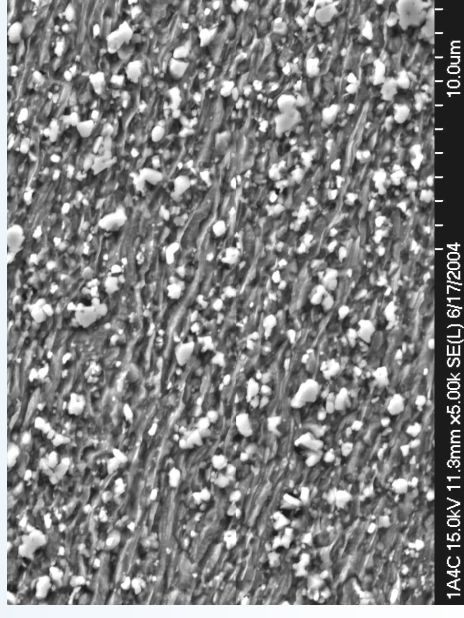


Roll Temp = 300 C, Total Red = 95 % , Roll Spd = 17 fpm

↔ Total Reduction ↔



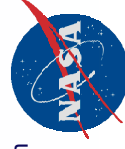
Roll Temp = 215 C, Total Red = 65 % , Roll Spd = 17 fpm



Roll Temp = 300 C, Total Red = 95 % , Roll Spd = 69 fpm

Roll Temp

Roll Speed



Summary

Warm Rolling Optimization Conclusions

- For the various levels of total reduction, rolling speed and strip rolling temperature representing boundaries of commercial processing, have slight to no influence on tensile properties.
- No second order effects were noted.
- Results indicate that the process conditions to roll strip for these variables can range over reasonable levels without any negative impact to performance.
- Incorporating broader process ranges in future rolling campaigns should lower commercial strip rolling costs by improving productivity.

Fabrication Summary

- GRCop-84 has a good combination of mechanical properties and exhibits exceptional stability when subjected to high temperature thermal cycles
- GRCop-84 can be easily formed and joined using conventional techniques for copper-based alloys
- GRCop-84 has the potential for many high temperature, high heat flux uses besides rocket engine liners